## CLAIMS

1.	High-st	cength	steel	sheet	excelle	nt	in	hole-
expandabil	lity and	ducti	lity, d	charact	erized	by;		

comprising, in mass%,

5 C: not less than 0.01 % and not more than 0.20 %, Si: not more than 1.5 %,

Al: not more than 1.5 %,

Mn: not less than 0.5 % and not more than

3.5 %,

10 P: not more than 0.2 %,

S: not less than 0.0005 % and not more

than 0.009 %,

N: not more than 0.009 %,

Mg: not less than 0.0006 % and not more

15 than 0.01 %,

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O: not more than 0.005 % and

Ti: not less than 0.01 % and not more than 0.20 % and/or Nb: not less than 0.01 % and not more than 0.10 %,

with the balance consisting iron and unavoidable impurities,

having the Mn%, Mg%, S% and O% satisfying equations (1) to (3), and

having the structure primarily comprising one or more of ferrite, bainite and martensite.

- $[Mg^{2}] \ge ([0^{2}]/16 \times 0.8) \times 24$  ... (1)
- $[S_{\delta}] \le ([Mg_{\delta}]/24 [O_{\delta}]/16 \times 0.8 + 0.00012) \times 32$  ... (2)
- $[S_{8}] \le 0.0075/[Mn_{8}]$  ... (3)
- 2. High-strength steel sheet excellent in hole-expandability and ductility described in claim 1, characterized by containing not less than  $5.0 \times 10^2$  per square millimeter and not more than  $1.0 \times 10^7$  per square millimeter of composite precipitates of MgO, MgS and (Nb, Ti)N of not smaller than 0.05  $\mu$ m and not larger than 3.0 $\mu$ m.
  - 3. High-strength steel sheet excellent in hole-

	expandability and ductility described in claim 1,
	characterized by having Al% and Si% satisfying equation
	(4).
	$[Si\%] + 2.2 \times [Al\%] \ge 0.35$ (4)
5	4. High-strength steel sheet excellent in hole-
	expandability and ductility described in claim 2,
	characterized by having Al% and Si% satisfying equation
	(4).
	$[Si\%] + 2.2 \times [Al\%] \ge 0.35$ (4)
10	5. High-strength steel sheet excellent in hole-
	expandability and ductility described in any of claims 1
	to 4, characterized by;
	having Ti%, C%, Mn% and Nb% satisfying
	equations (5) to (7),
15	having the structure primarily comprising
	bainite, and
	having a strength exceeding 980 N/mm <sup>2</sup> .
	$0.9 \le 48/12 \times [C_8]/[Ti_8] < 1.7$ (5)
	$50227 \times [C%] - 4479 \times [Mn%] > -9860$ (6)
20	811×[C%]+135×[Mn%]+602×[Ti%]+794×[Nb%]>465 (7)
	6. High-strength steel sheet excellent in hole-
	expandability and ductility described in any of claims 1
	to 4, characterized by;
	having C%, Si%, Al% and Mn% satisfying
25	equation (8),
	having the structure primarily comprising
	ferrite and martensite, and
	having a strength exceeding 590 $N/mm^2$ .
	$-100 \le -300$ [C%] +105 [Si%] -95 [Mn%] +233 [Al%] (8)
30	7. High-strength steel sheet excellent in hole-
	expandability and ductility described in claim 6,
	characterized in that;
	not less than 80 % of crystal grains
	having a short diameter (ds) to long diameter (dl) ratio
35	(ds/dl) of not less than 0.1 exist in the steel
	structure.

8. High-strength steel sheet excellent in hole-expandability and ductility described in claim 7, characterized in that;

not less than 80 % of ferrite crystal grains having a diameter of not less than 2  $\mu m$  exist in the steel structure.

- 9. High-strength steel sheet excellent in hole-expandability and ductility described in any of claims 1 to 4, characterized by;
- having C%, Si%, Mn% and Al% satisfying equation (8),

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having the structure primarily comprising ferrite and bainite, and

having the strength exceeding 590 N/mm<sup>2</sup>.

-100≤-300[C%]+105[Si%]-95[Mn%]+233[Al%] ... (8)

10. High-strength steel sheet excellent in hole-expandability and ductility described in claim 9, characterized in that;

not less than 80 % of crystal grains having a short diameter (ds) to long diameter (dl) ratio (ds/dl) of not less than 0.1 exist in the steel structure.

11. High-strength steel sheet excellent in hole-expandability and ductility described in claim 10, characterized in that;

not less than 80 % of ferrite crystal grains having a diameter of not less than 2  $\mu m$  exist in the steel structure.

12. A method for manufacturing high-strength steel sheet excellent in hole-expandability and ductility, which has the structure primarily comprising ferrite and martensite and a strength in excess of 590 N/mm², characterized by the steps of;

completing the rolling of steel having a composition described in any of claim 1 to 4 at a finish-rolling temperature of not lower than the  ${\rm Ar}_3$ 

transformation point,

cooling at a rate of not less than 20 °C/sec, and

coiling at a temperature below 300 °C.

- 5 13. A method for manufacturing high-strength steel sheet, excellent in hole-expandability and ductility, which has the structure primarily comprising ferrite and martensite and a strength in excess of 590 N/mm², characterized by the steps of;
- completing the rolling of steel having a composition described in any of claims 1 to 4 at a finish-rolling temperature of not lower than the  ${\rm Ar}_3$  transformation point,

cooling to between 650 °C and 750 °C at a rate of not less than 20 °C/sec,

air-cooling at said temperature for not longer than 15 seconds,

re-cooling, and

coiling at a temperature below 300 °C.

- 14. A method for manufacturing high-strength steel sheet, excellent in hole-expandability and ductility, which has the structure primarily comprising ferrite and bainite and a strength in excess of 590 N/mm<sup>2</sup>, characterized by the steps of;
- completing the rolling of steel having a composition described in any of claims 1 to 4 above at a finish-rolling temperature of not lower than the  $Ar_3$  transformation point,

cooling at a rate of not less than 20

30 °C/sec, and

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coiling at a temperature of not lower than 300  $^{\circ}\text{C}$  and not higher than 600  $^{\circ}\text{C}\,.$ 

15. A method for manufacturing high-strength steel sheet excellent in hole-expandability and ductility, which has the structure primarily comprising ferrite and bainite and a strength in excess of 590 N/mm<sup>2</sup>,

characterized by the steps of;

completing the rolling of steel having a composition described in any of claims 1 to 4 above at a finish-rolling temperature not lower than the  ${\rm Ar}_3$  transformation point,

cooling to between 650 °C and 750 °C at a rate of not less than 20 °C/sec,

 $\mbox{air-cooling at said temperature for not} \\ \mbox{longer than 15 seconds,}$ 

10 re-cooling, and

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coiling at a temperature of not lower than 300  $^{\circ}\text{C}$  and not higher than 600  $^{\circ}\text{C}$  .